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Corrigendum

Corrigendum to "Uniaxial viscosity of gadolinium-doped ceria determined by discontinuous sinter forging" [J. Eur. Ceram. Soc. 27 (2007) 3127–3133]

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The authors regret that typing errors occurred in the published article indicated above. The corrections are shown below:
A.3. Riedel et al. [15]
For the intermediate stage of sintering ($Z=8$):

$$K_p^1(\rho) = (\alpha_0 + \alpha_1\psi + \alpha_2\psi^2) + (\beta_0 + \beta_1\psi + \beta_2\psi^2)(1-\rho) + (\gamma_0 + \gamma_1\psi + \gamma_2\psi^2)(1-\rho)^2$$

where ψ is the equilibrium dihedral angle.
For the final stage of sintering:

$$K_p^1(\rho) = \frac{1}{144\rho}\left(-2\,\ln(\xi\omega) - \frac{33}{64} + \xi\omega - \frac{(\xi\omega)^2}{16}\right)$$

where $\xi = 4.063$ is a geometry factor,

$$\omega(\rho,\psi) = 6^{1/3}\left(\frac{1-\rho}{4h(\psi)}\right)^{2/3}$$

and

$$h(\psi) = \frac{(1+\cos(\psi/2))^{-1} - 1/2\,\cos(\psi/2)}{\sin(\psi/2)}$$

$G_p^1(\rho)$ is calculated from:

$$\frac{G_p^1}{K_p^1}(\rho) = [0.27 + 2(\rho - 0.602)^2]\left[1 - \left(\frac{0.4}{1.4-\rho}\right)^{12}\right]$$

Finally

$$E_p^1(\rho) = \frac{9K_p^1 G_p^1}{3K_p^1 + G_p^1}$$

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A.4. Venkatachari et al. [33]

$$G_p = G_p^0 d^3 \rho$$

$$K_p = K_p^0 d^3 \frac{1}{\rho}[\ln(1-\rho) + 0.5\rho(\rho+2)]$$

$$E_p^1(\rho) = \rho \frac{9\ \ln(1-\rho) + 0.5\rho(\rho+2)}{3K_p^0/\rho([\ln(1-\rho) + 0.5\rho(\rho+2)] - G_p^0\rho)}$$